

Design of high silicon steel for motors and electronics

Sandia Power Electronics and Energy Conversion Workshop 2023

Presentation Date: August 3rd, 2023

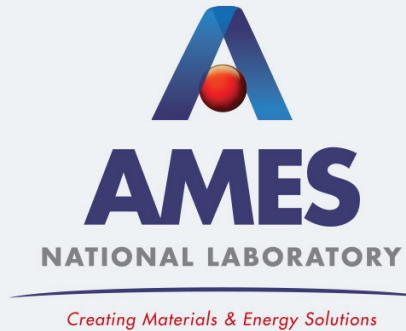
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Ames National Laboratory

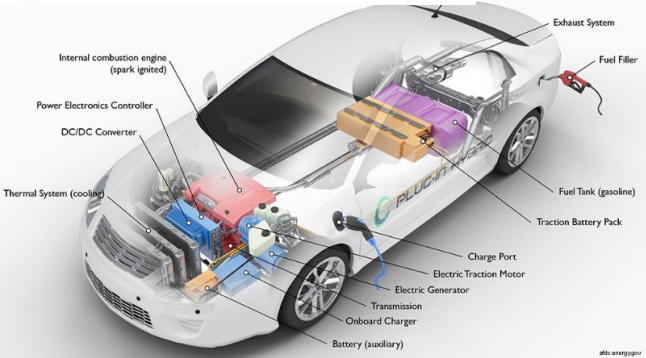
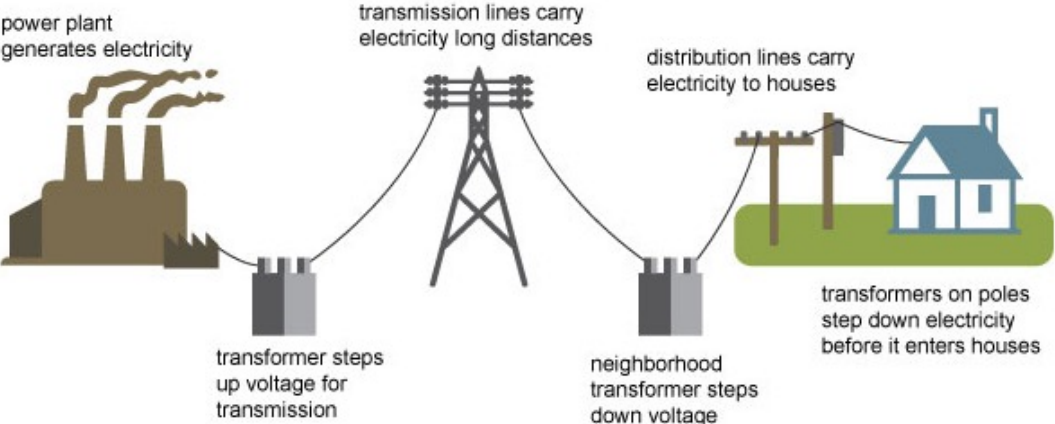
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Soft magnet materials (SMMs) and clean energy

Electricity generation, transmission, and distribution



Applications of SMMs

Transformer cores



Electrical machines (motors and generators)



Inductor cores



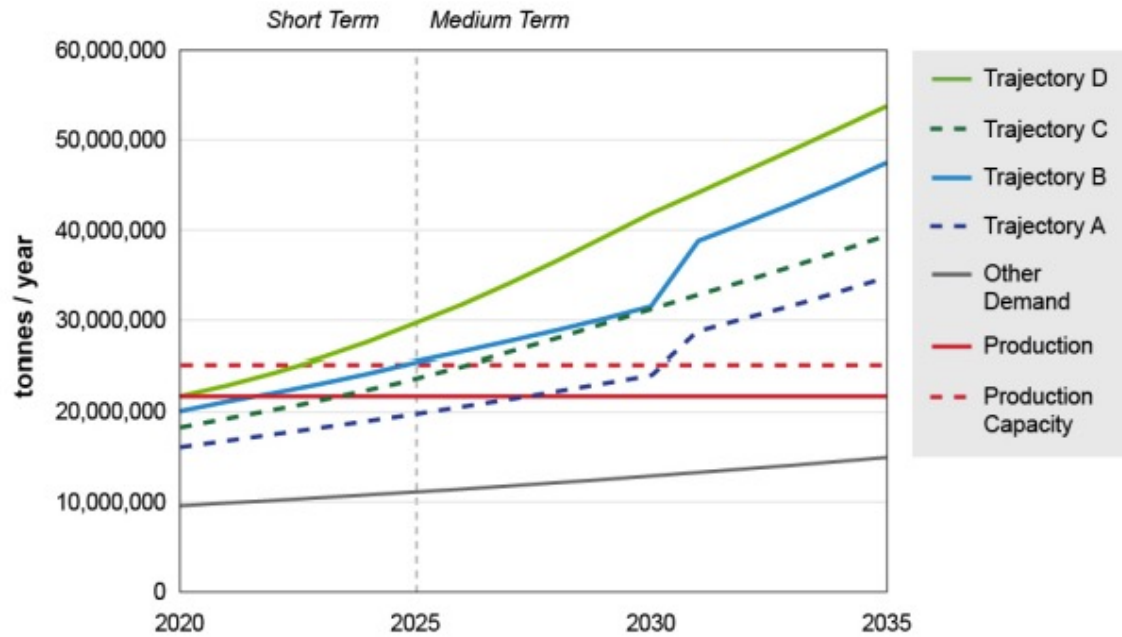
Material	Application	Materials Intensity
Electrical steel	Vehicle motor	40-100 kg per vehicle
	Transformer	72,570 – 108,860 kg/unit of large power transformer
	Wind	1,360 – 4,810 kg/MW for onshore application 2,450 – 3,470 kg/MW for offshore application

Ref: U.S. Department of Energy, Critical Materials Assessment 2023

- Soft magnetic materials are needed for transformers for the grid and motors in EV

SMMs are in great demand

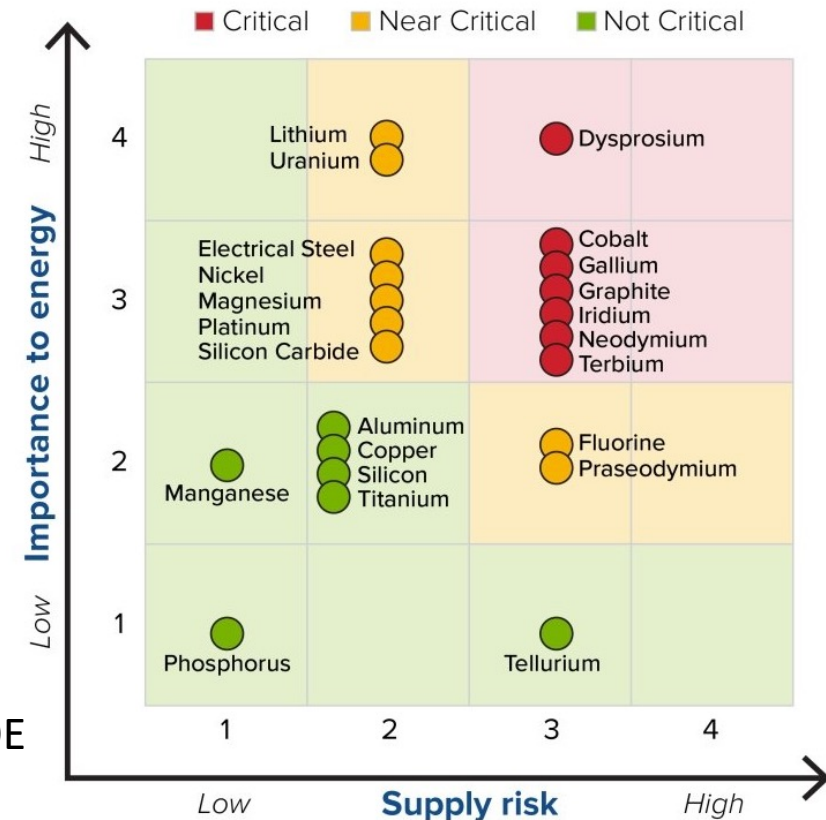
ELECTRICAL STEEL FUTURE DEMAND AND HISTORIC SUPPLY



Ref: U.S. Department of Energy, Critical Materials Assessment 2023

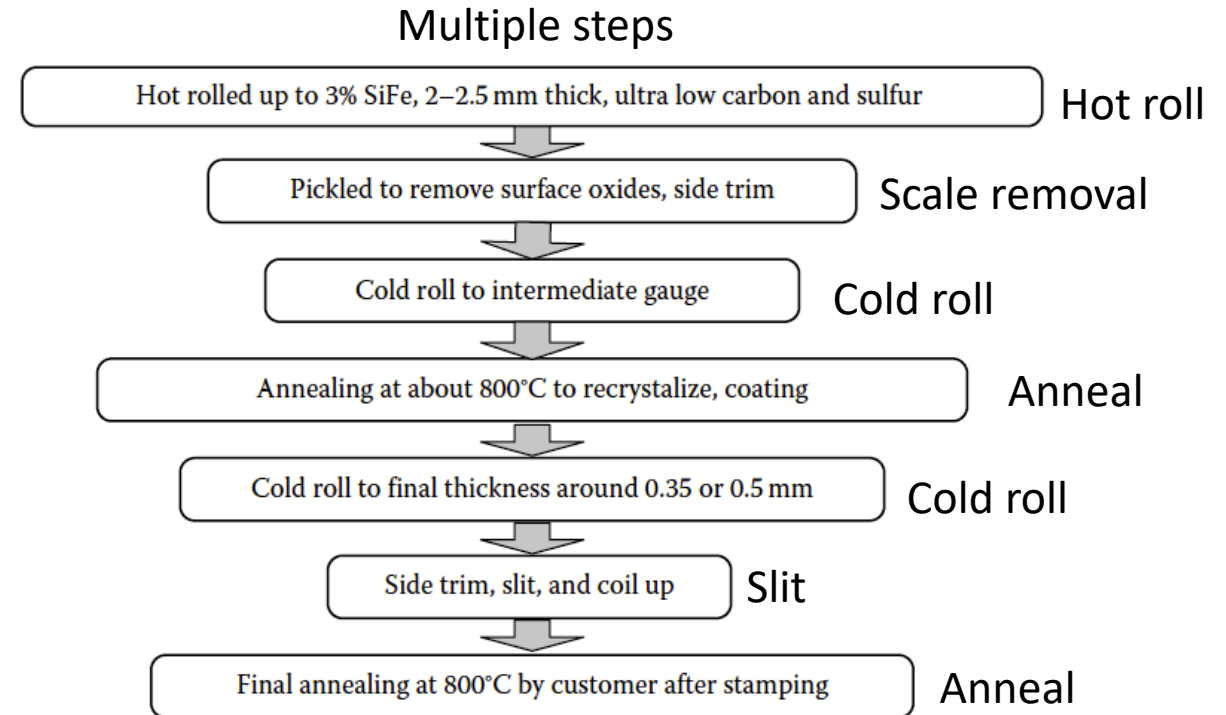
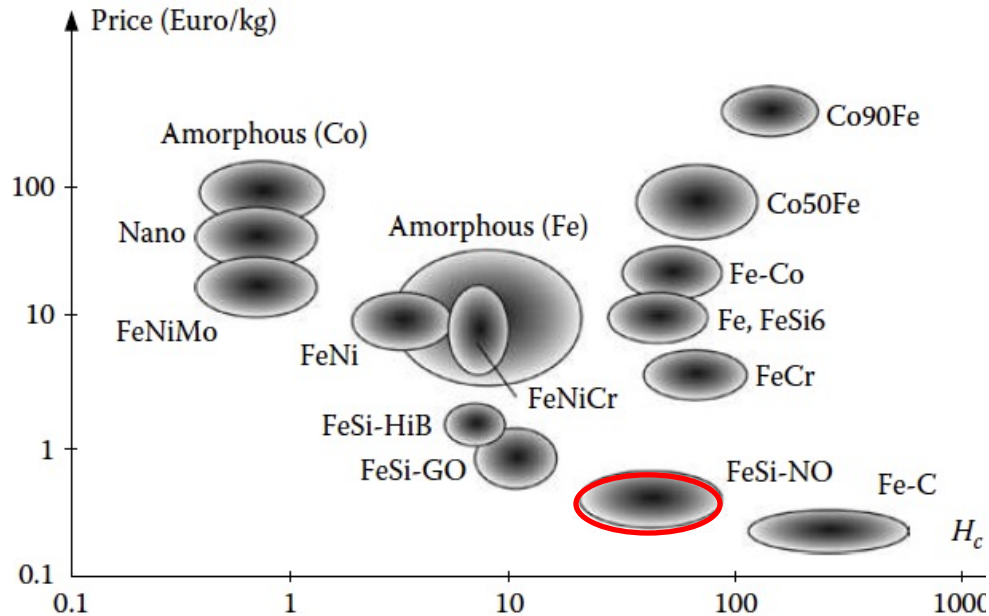
- Electrical steel has been identified as critical materials by US DOE
- Huge demand for soft magnetic materials

SHORT TERM 2020-2025



Ref: U.S. Department of Energy, Critical Materials Assessment 2023

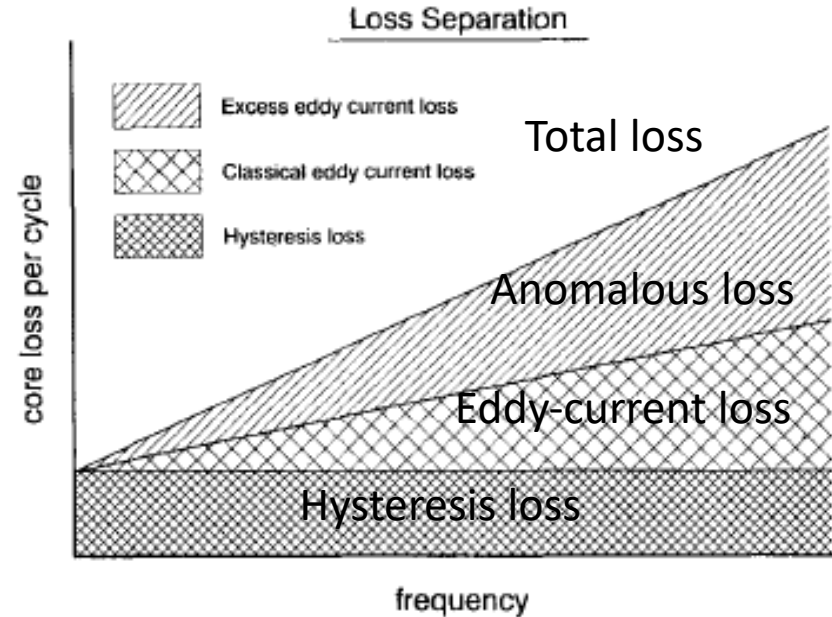
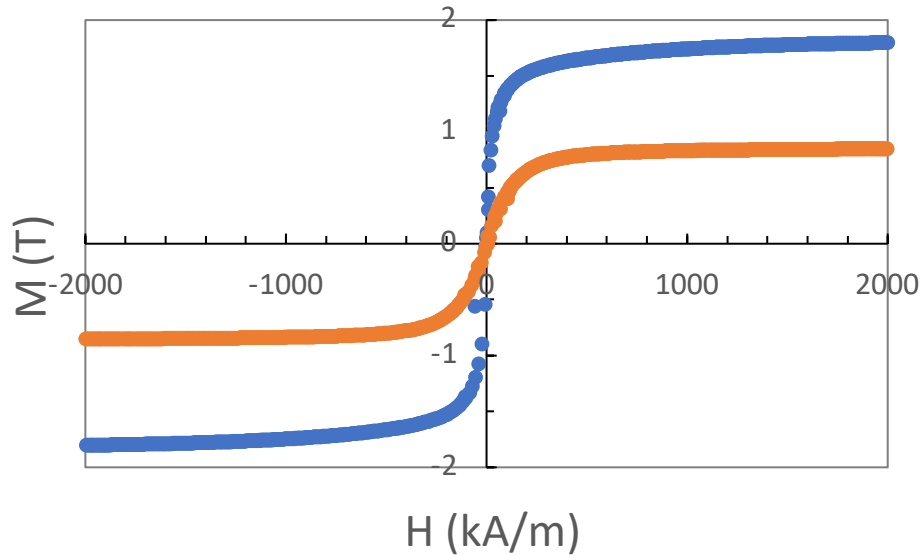
Cost and processing of SMMs



Ref: Tumanski, S. *Handbook of magnetic measurements*. (CRC press, 2016).

- Both cost of raw materials and the cost of processing are important for soft magnetic materials

Power density and efficiency of SMMs



Flux density

Thickness

Frequency

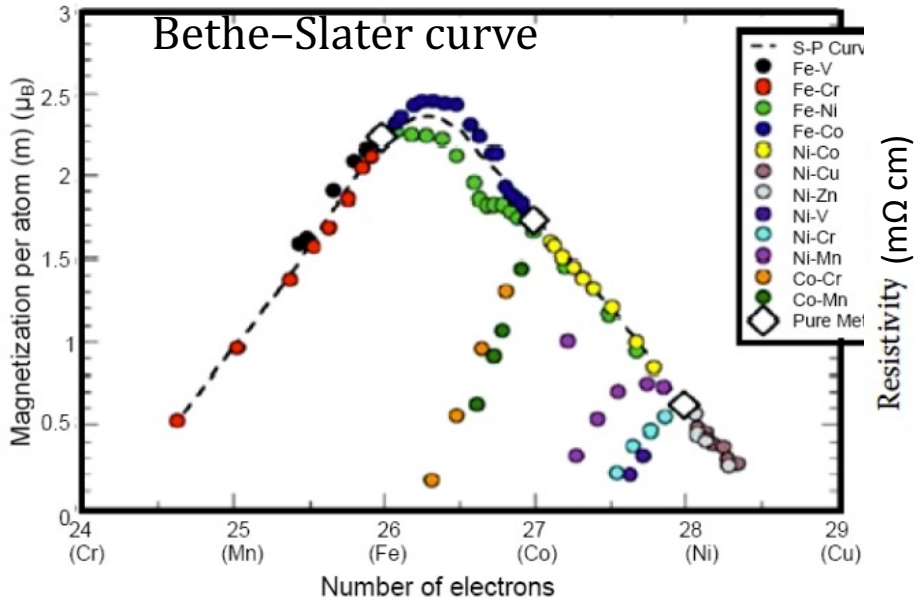
$$P_{eddy} = \frac{10^{-9} \pi^2 d^2 B_0^2 f^2}{6\rho}$$

Resistivity

- Higher saturation magnetization leads to high power density.
- Higher f increase power density, significantly reduces motor size.
- Higher f is beneficial only if new soft magnetic materials can keep the loss low.
- SMMs with high saturation and high resistivity are needed.

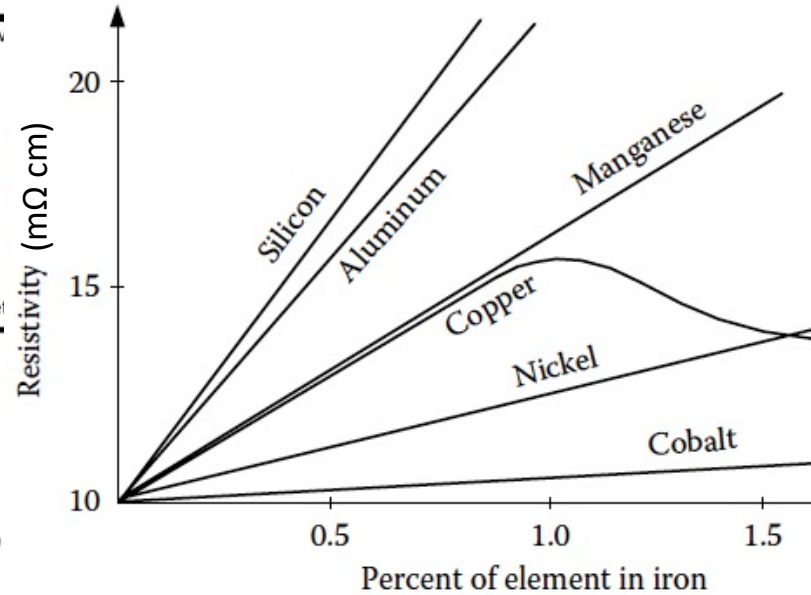
Aspects for designing of SMM

Saturation



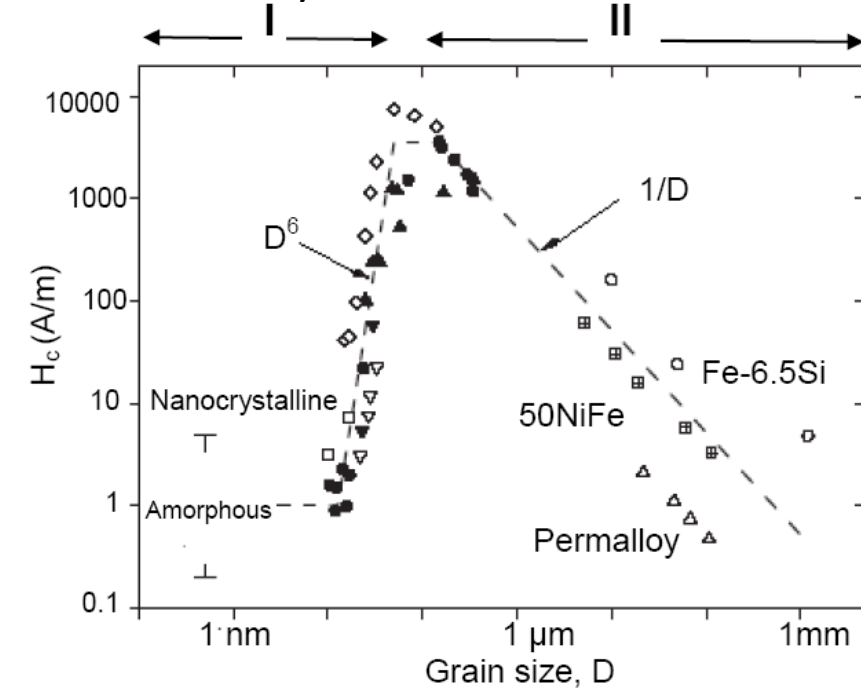
Ref: Roy et al. Alloy Development through Rapid Solidification for Soft Magnetic Application

Resistivity



Ref: Tumanski, S. Handbook of magnetic measurements. (CRC press, 2016).

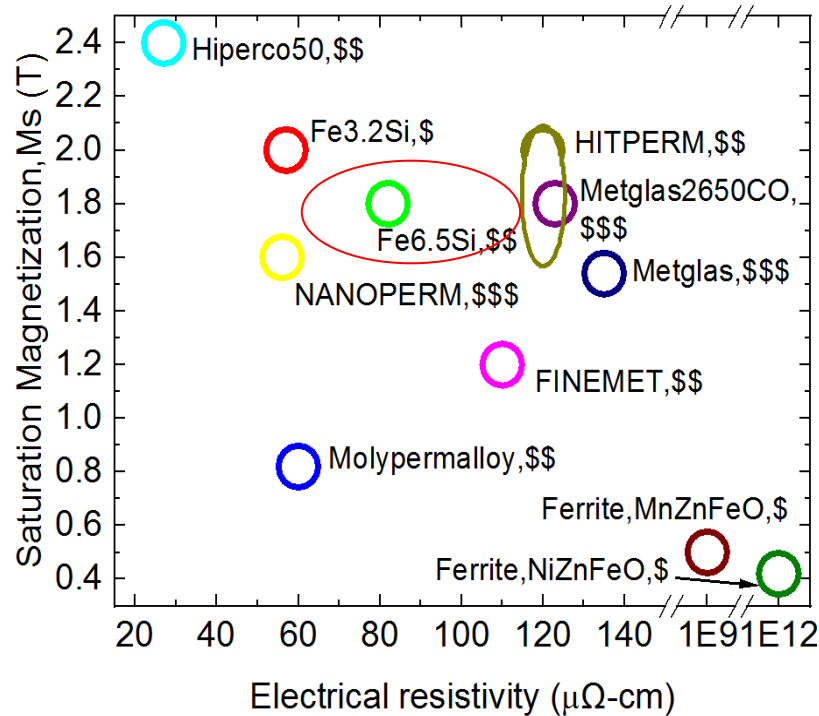
Coercivity



G. Herzer coercivity grain size relationship

- SMM can be designed through compositions and processing

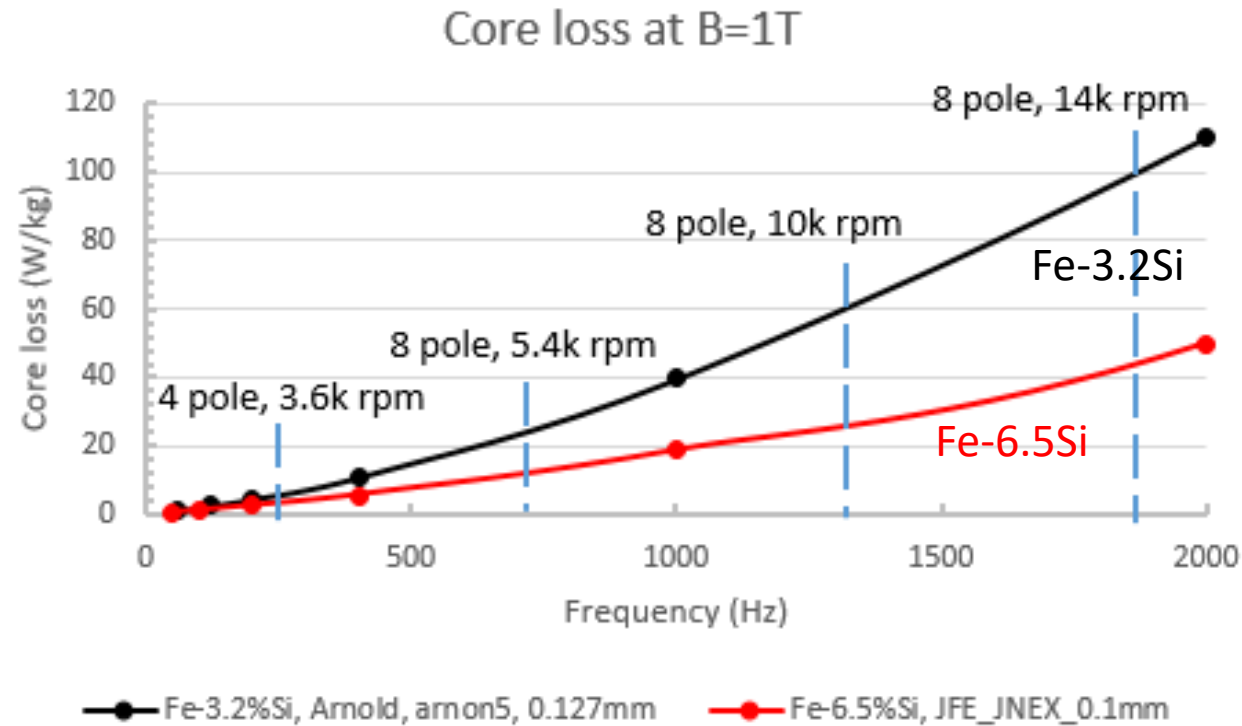
Overview of SMM and high silicon steel



- Fe-3.2%Si steel offers the most attractive cost/performance ratio
- Fe-6.5%Si Electric steel offers both high flux density and high electric resistivity.
- Fe-6.5%Si offers lower eddy current, smaller hysteresis loss, nearly zero magnetostriction.

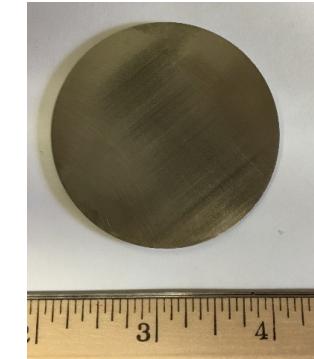
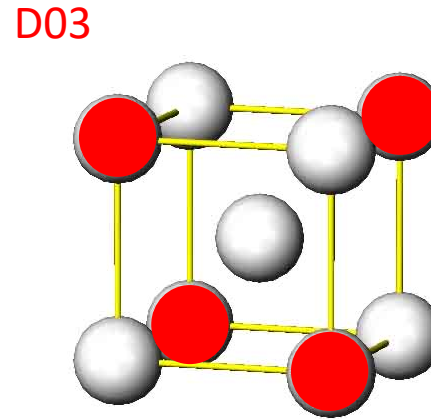
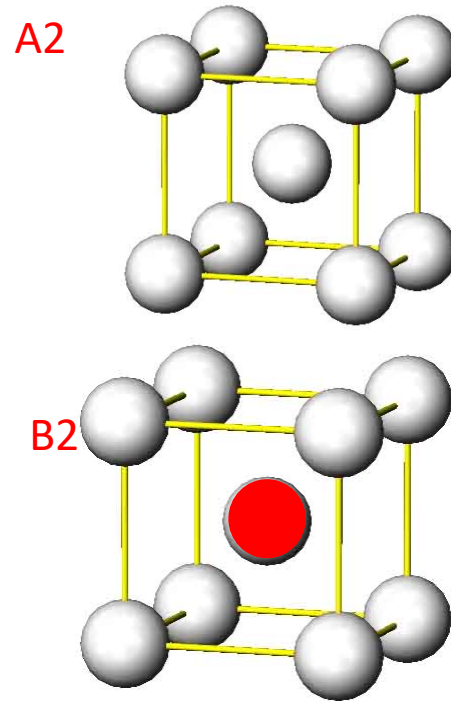
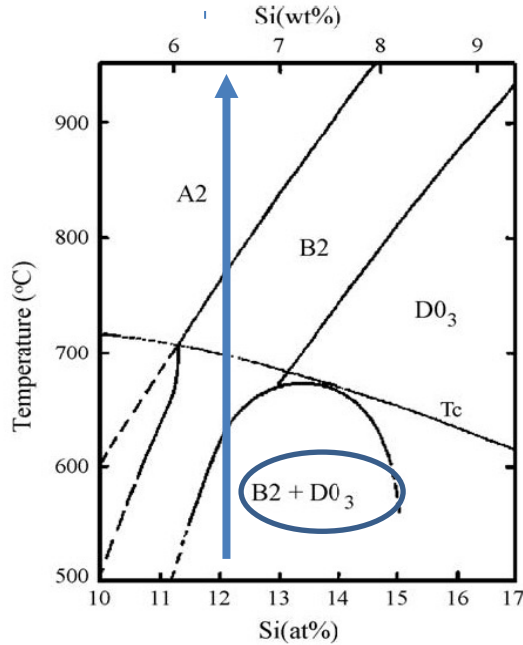
Materials (\$\$ additions)	Bs (T)	Hc (A/m)	$10^3\mu_r$ 1 kHz	R ($\mu\Omega\text{-cm}$)	λ (ppm)	$W_{1.5/50}$ (W/kg)	$W_{10/400}$ (W/kg)
Electrical Steel, 0.2mm, NGO, 3.2% Si	2	26	15	57	8	0.7-1.2	11
Electrical Steel, 0.2mm, NGO, 6.5% Si	1.8	20	19	82	0.01	0.6	8.1
Molypermalloy, 0.5mm, Ni78Fe17Mo5	0.65-0.82	0.25-0.64	100-800	60	2-3	0.07	0.3
Hiperco 50, Fe49Co49V2	2.4	16-400	5-50	27	60	4	10
FINEMET, Fe73.5Si13.5Nb3B6Cu1	1.2	0.5-1.4	80	110	0-2	--	1.1
NANOPERM, Fe88B4Zr7Cu1	1.5-1.6	2.4-4.5	48	56	~0	--	3
HITPERM, (FeCo)44Zr7B4Cu1	1.6-2.0	80-200	1-10	120	36	--	20
Metglas, Fe78Si9B13	1.54	3	2.1	135	27	0.7	2-5
Metglas 2650CO, Fe67Co18B14Si1	1.8	3.5	50	123	35	0.3	3

Comparison of Fe-6.5Si over Fe-3.2Si



- Fe-6.5Si offers significant lower iron losses than Fe-3.2Si, especially at high frequencies

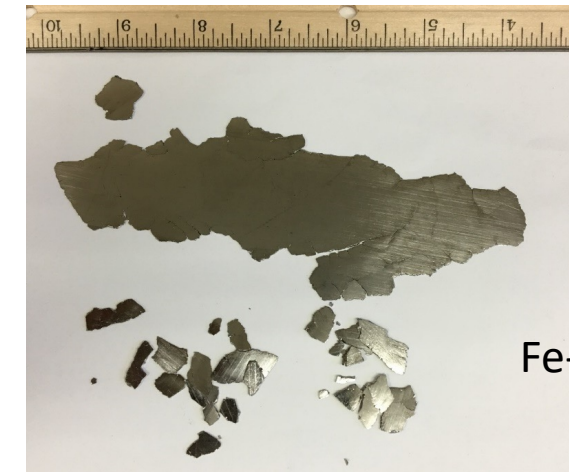
Challenges in Fe-6.5Si (ordering)



Fe-6.5Si



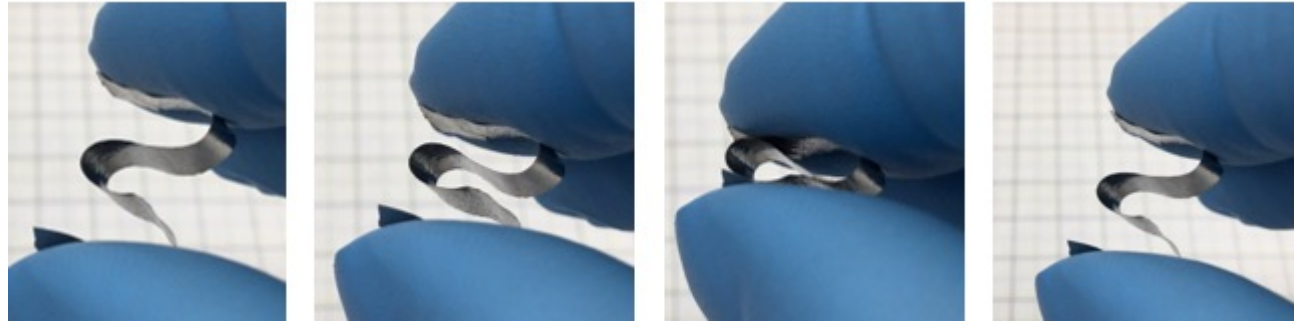
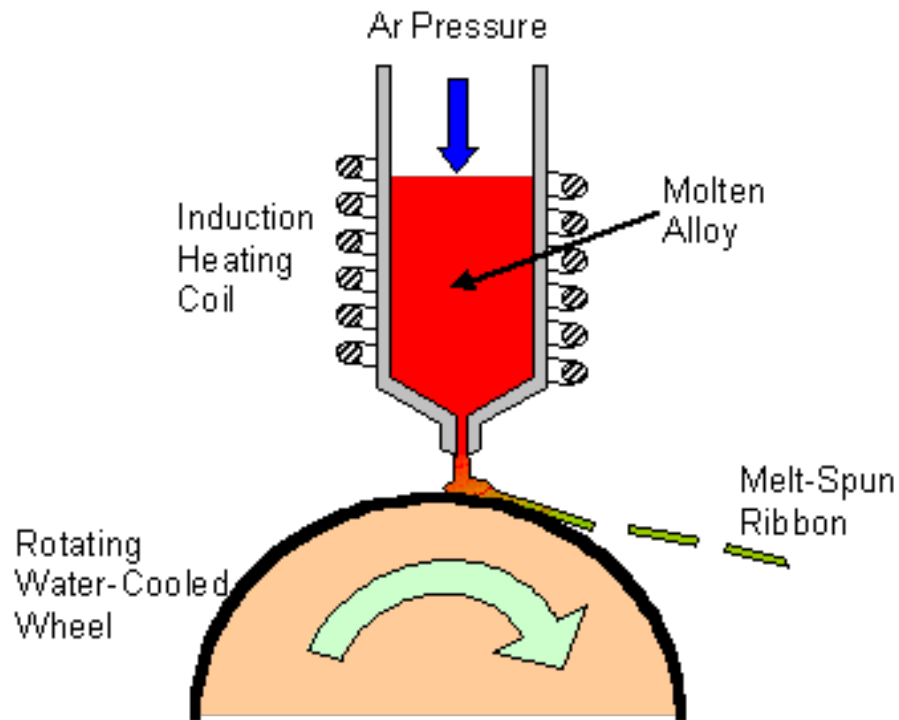
Cold roll



Fe-6.5Si

- Fe-6.5Si lies in the B2/D0₃ two phase region.
- B2 and D0₃ ordering results in brittleness. resulted from ordering of nearest neighbor and next-nearest-neighbor atoms.
- B2 and D0₃ ordering results in brittleness.
- Fe-6.5Si can not be cold rolled.

Rapid solidification suppresses the ordering



Time lapse of a video



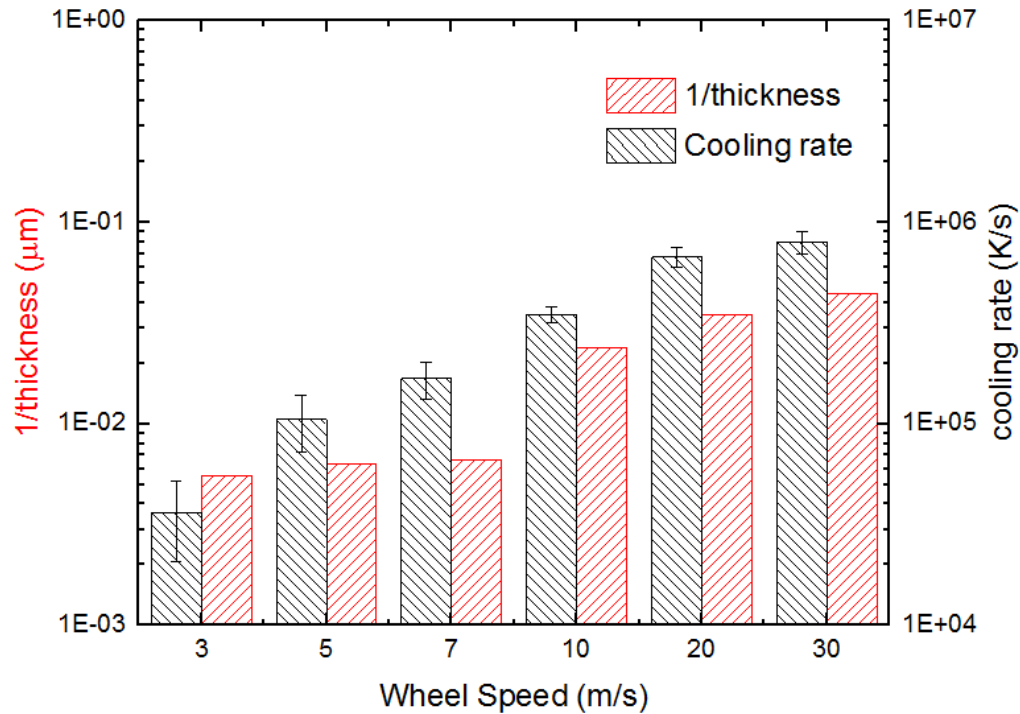
Heavy spur implies the material is too ductile

Rapid solidification of Fe-6.5Si bypasses the ordered phases resulting in ductility.

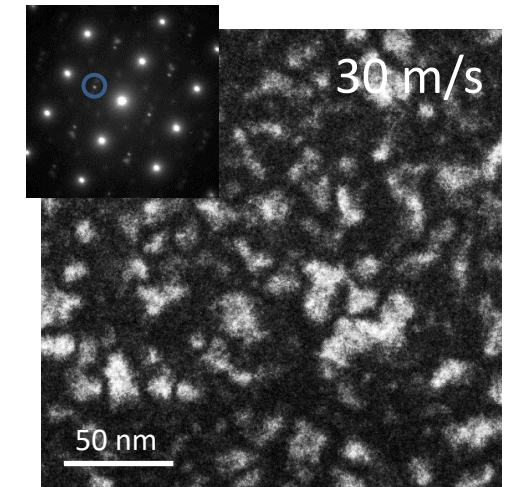
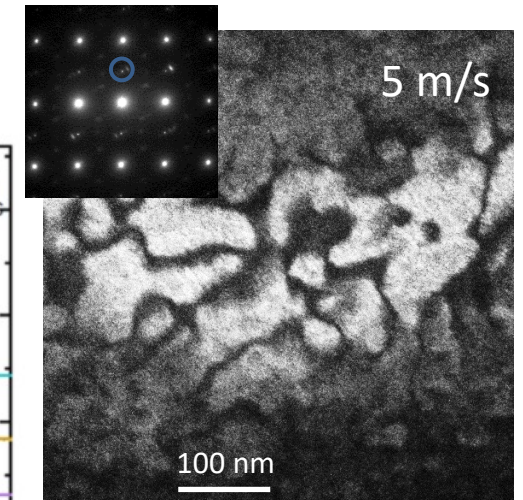
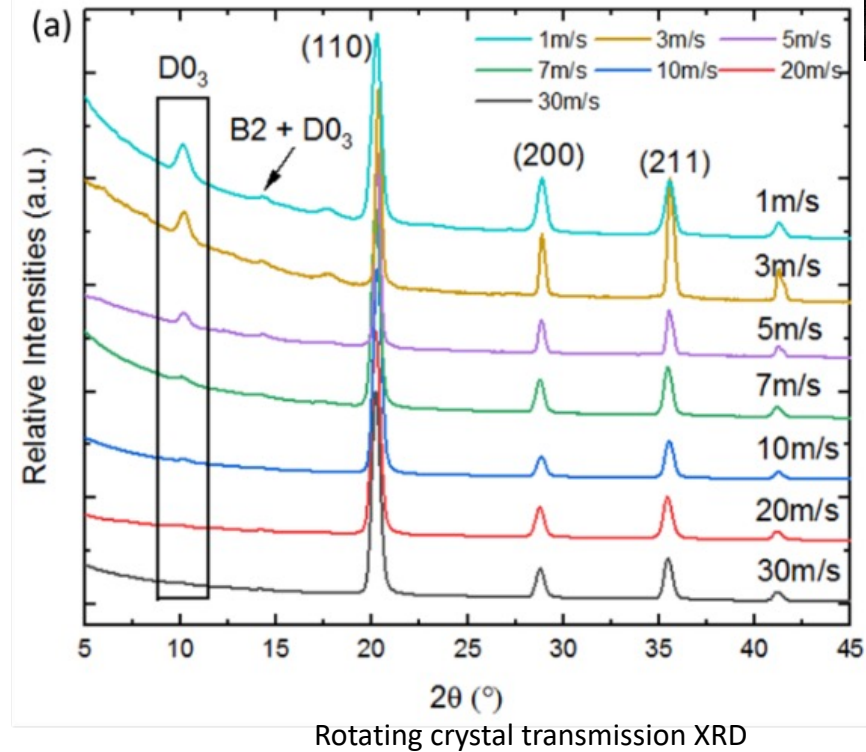
- Can the property of Fe-6.5Si be adjusted by varying the cooling rate/wheel speed?
- How can we use rapid solidified Fe-6.5Si?

Cooling rates and Fe-6.5Si ordering

Tuning long range order through varying cooling rates

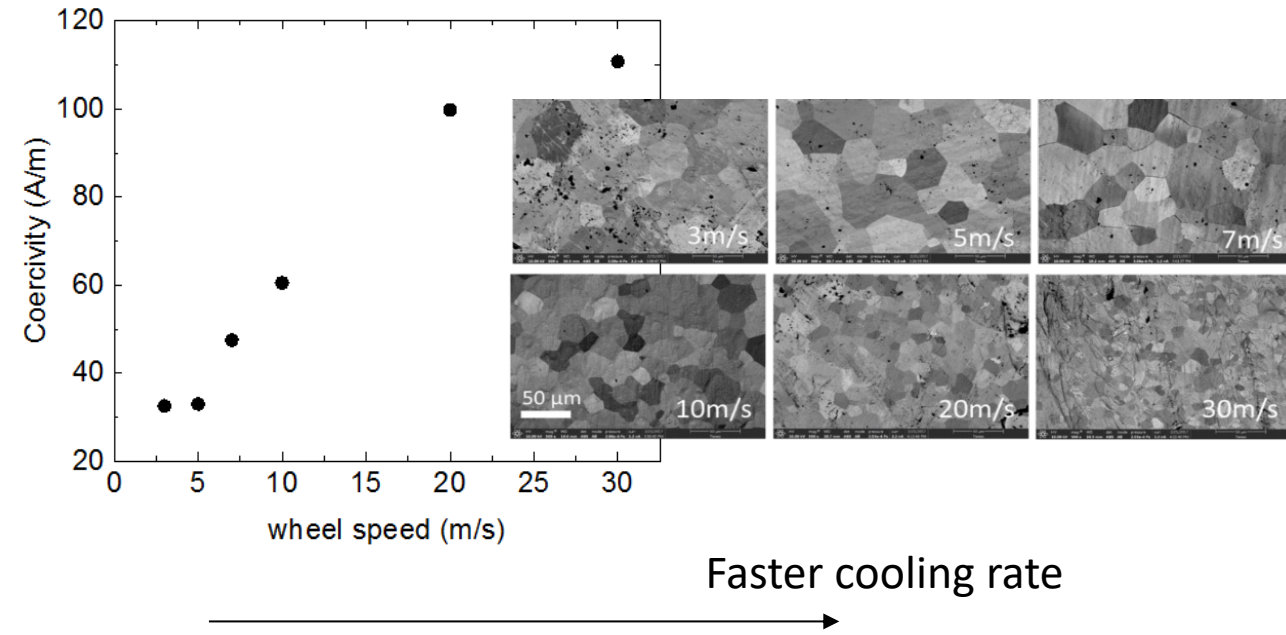
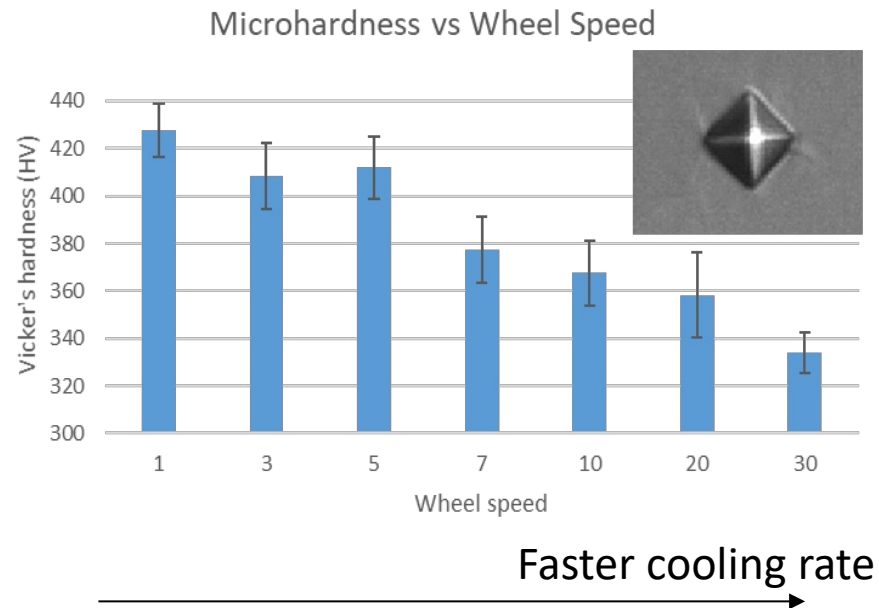


Long range order characterization



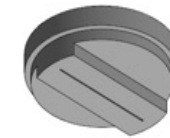
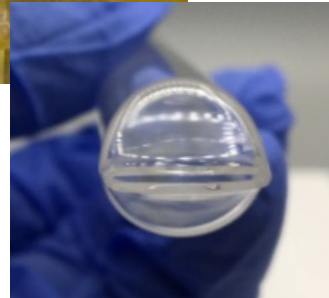
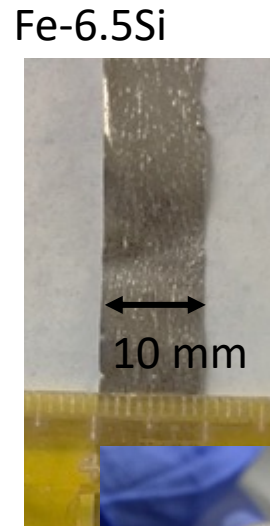
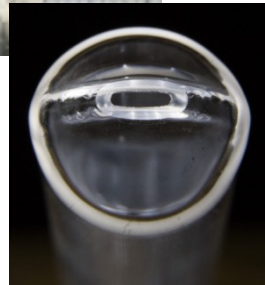
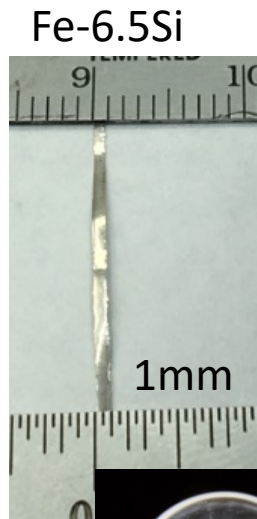
- Cooling rate and ribbon thickness effectively tuned by adjusting the wheel speed.
- Faster cooling results in lower degree of ordering of Fe-6.5Si and smaller ordered domain size.

Cooling rates and Fe-6.5Si physical properties



- Ductile Fe-6.5Si ribbon beyond 7m/s due to lower degree of ordering.
- Coercivity is affected by different grain size on as spun Fe-6.5Si.

Fe-6.5Si ribbon/tape for tape wound cores

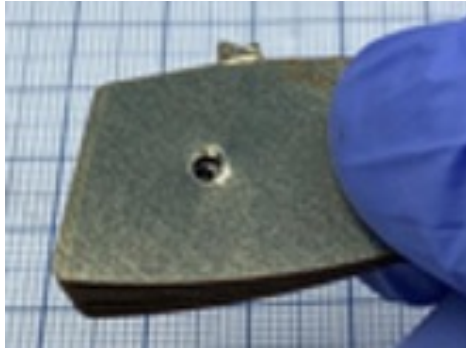


Tape wound cores

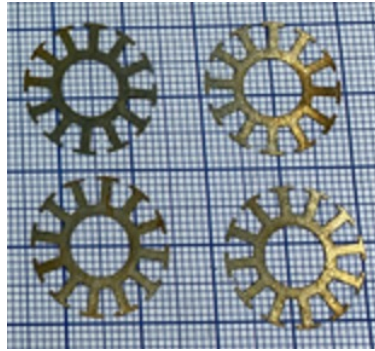
- Width of the ribbon increased from 1mm to 10mm.
- Consistently producing 6 mm wide 0.1mm thick Fe-6.5Si ribbons using small melt spinner.
- Currently working on further increase the width to 50mm.

Fe-6.5Si tape for motor laminates

Fe-6.5Si motor demon



Fe-6.5Si



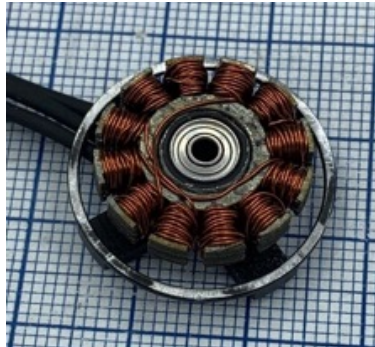
EDM



Laminating



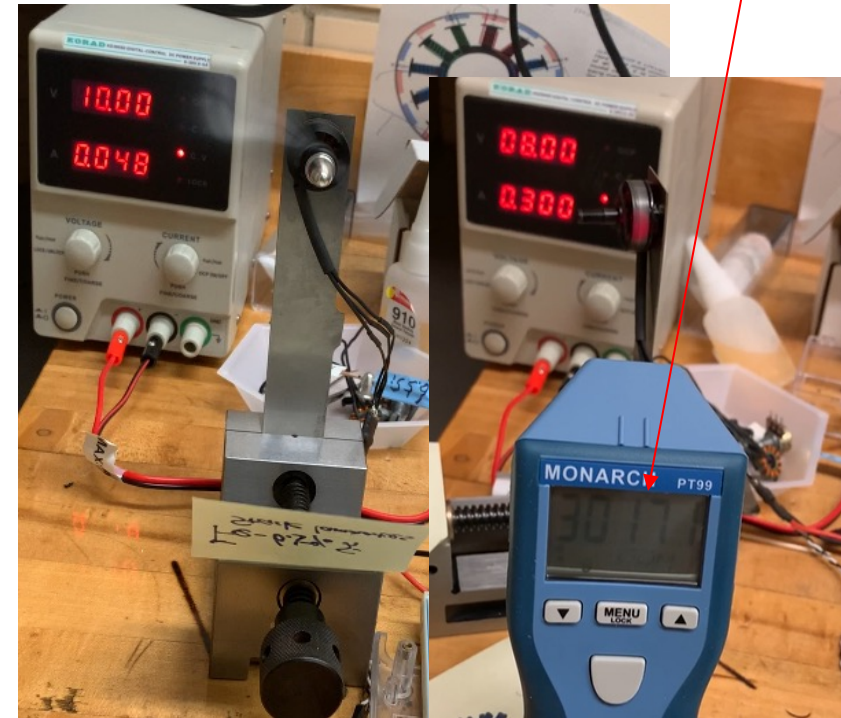
Winding



Stator



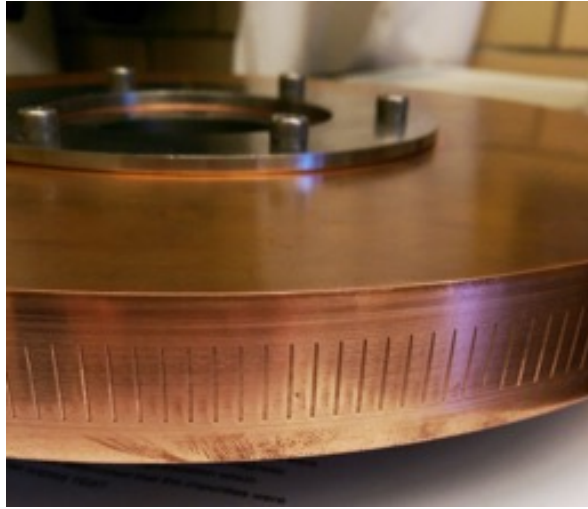
PM rotor



Running with ESC

- Fe-6.5Si laminates/tapes can be machined for stator laminates for motors.

Fe-6.5Si flake production

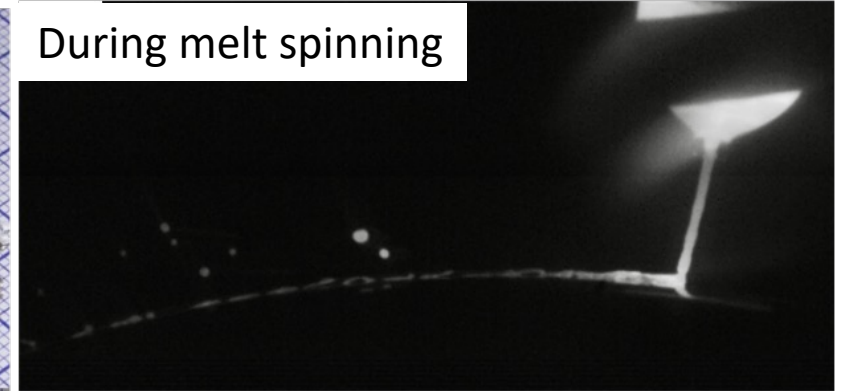


Grooved wheel breaking continuous ribbon to flakes

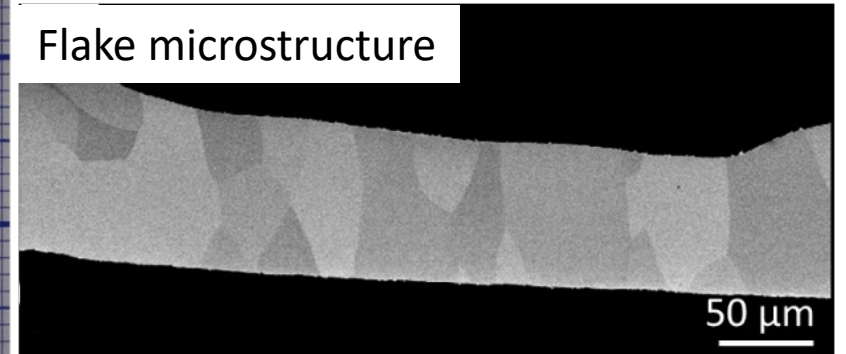
Melt spun flakes



During melt spinning



Flake microstructure



- Successful production of flakes ~ 0.1 mm thickness, 1mm width and 2mm length.
- The waste can be used as raw material to melt spun more flakes, eliminating waste.

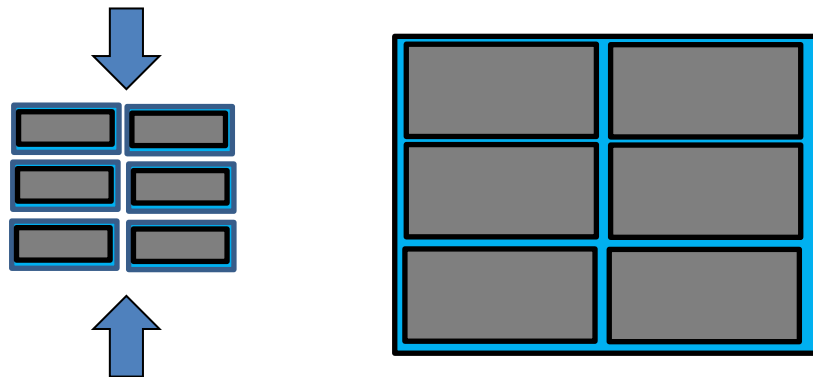
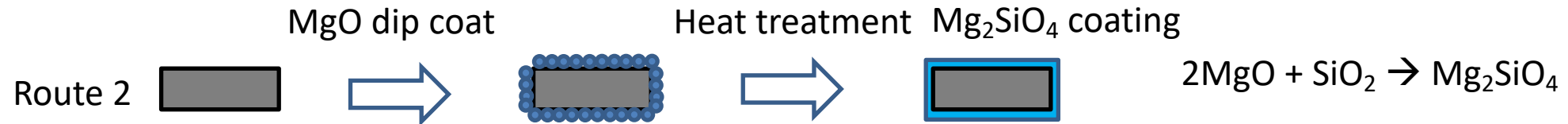
Performance of flake-based Fe-6.5Si



		Ameslab GO2P23	NO Si steel	Ameslab GO2P23	JNHF	Ameslab GO2P23	JNEX
		Fe-6.5Si	Fe-3.2Si	Fe-6.5Si	Gradient Fe- 6.5Si	Fe-6.5Si	Fe-6.5Si
thickness	(mm)	0.33	0.35	0.2	0.2	0.1	0.1
W10/400	(W/kg)	10.8	14.4	7.2	14.5	6.1	5.7
W10/1k	(W/kg)	45.7	62.0	27.3	29.1	20.2	18.7
DC, μ Max		28.7k	18.0k	28.4k	3.9K	25.8k	23.0k

- The hot pressed sample suffered from poor AC magnetic properties (high iron loss).
- Fe-6.5Si has lower losses than the traditional Fe-3.2%Si with the same thickness.
- Our 0.2mm sample achieved record low iron loss at 400Hz and 1000Hz.
- Our 0.1mm sample has W10/400 of 6.1W/kg.

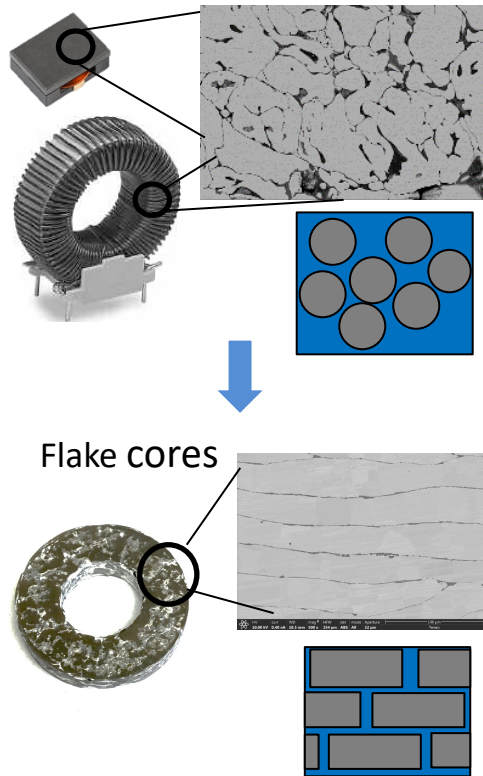
Flake lamination and assembly



- Coating + Shaping
 - Solution coating of CaF_2
 - Dip coat of MgO
 - MgO powder co pack anneal
 - Si-B powder co-pack cementation
 - Epoxy solution coat

The comparison of flake cores and powder core

Current state of the art:
Powder based cores



Flake core vs. powder core

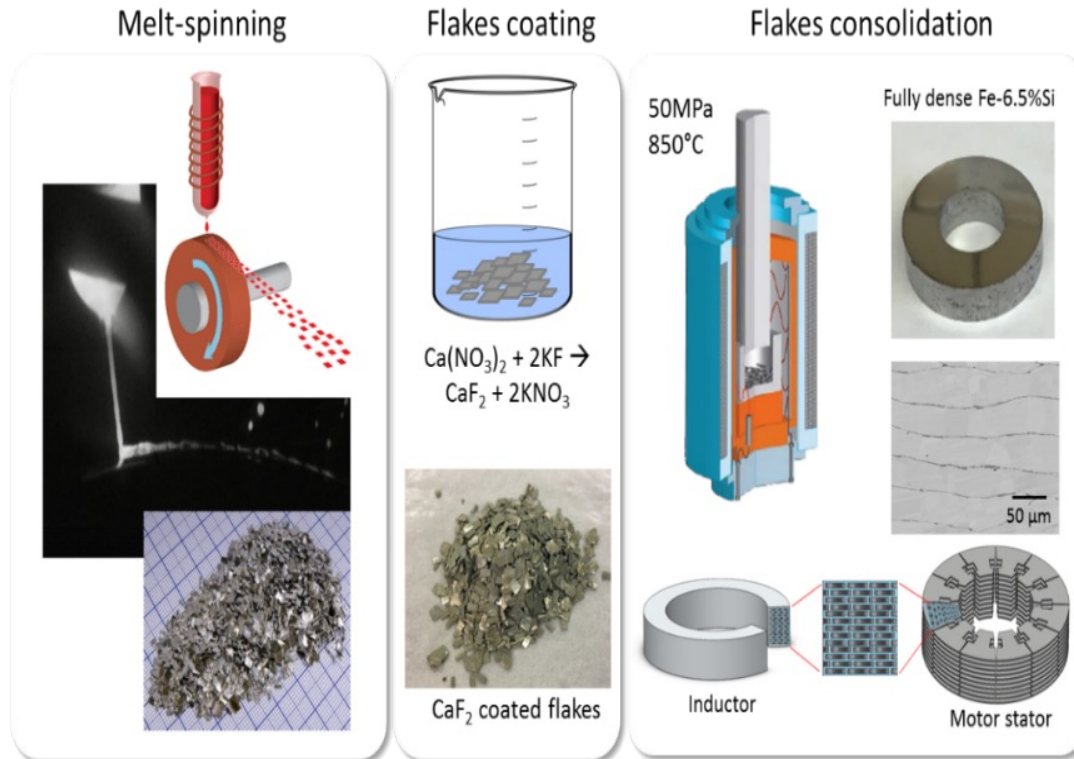
Flux density	AC/Iron Loss (W/kg)						DC		
	0.1T		0.2T		0.5T				
Frequency, Hz	Powder Core	Flake Core	Powder Core	Flake Core	Powder Core	Flake Core		Powder Core	Flake Core
50	0.14	0.05	0.48	0.18	2.33	0.87	B8, T	0.04	0.09
60	0.14	0.07	0.72	0.26	2.84	0.99	B15, T	0.07	0.16
100	0.32	0.12	1.19	0.43	4.87	1.83	B50, T	0.22	0.46
400	1.37	0.55	4.78	1.92	20.03	8.72	B80, T	0.34	0.64
1000	3.53	1.56	12.32	5.65	53.41	26.68	umax	35.90	86.75

Powder diameter = flake thickness; 5wt%epoxy binder

- Flake core shows improvement in magnetic properties than powder core.

Summary

➤ Significant demand for SMMs



Fe-6.5%Si

Low cost

High performance

No supply chain issue

Low carbon output processing

- Cooling rate determines Fe-6.5%Si properties.
- Fe-6.5%Si can be used as wide ribbon, flakes, and ribbons format.
- Fe-6.5%Si flakes enable near net shape processing, and good magnetic properties.

Questions: Gaoyuan Ouyang, gaoyuan@iastate.edu

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