

Overcoming Materials Challenges for SFR sCO₂ EC Systems

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In-Situ Corrosion Monitoring System

Two activities are underway to continue the exciting developments of in-situ alloy corrosion monitoring capability in sCO₂ systems. Two large high temperature corrosion furnaces, used in FY17 for alloy corrosion experiments, are being modified to incorporate multiple in-situ electrical resistance corrosion probes. Experiments will be performed to validate measured corrosion rates versus those for witness samples of the same alloys. Prior to implementing in-situ corrosion monitors in sCO₂ systems, the ability of the probes to operate within a high pressure environment needs to be evaluated. A corrosion probe will undergo testing in the new high pressure test facility at Sandia-NM to ensure that it is able to withstand this environment.



In-situ Electrical Resistance (ER) Corrosion Probe



High temperature corrosion furnaces (setup / used in FY17 corrosion tests)

High Temperature (>550°C) Bearing Coatings

Recent discussions with Industry have identified the need for gas foil bearing coating material solutions at higher temperatures (>550°C). For this work, we are collaborating with industry (Xdot and LiquidMetal Coatings) to identify and evaluate up to 6 different high temperature bearing coating materials at 2 different Temperatures for 500hr durations in high pressure CO₂. Down-selected materials would be candidates for future bearing tests by Xdot and/or Sandia.

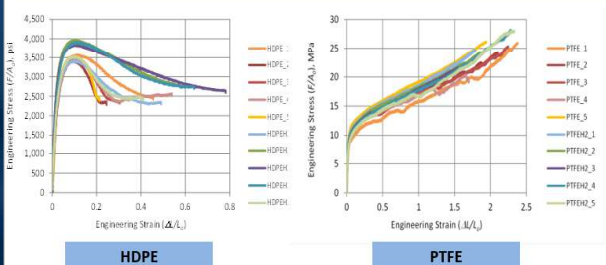


sCO₂ / Polymer Interactions

Polymer bushings and O-rings are used in low temperature system equipment/components such as valves. Very little is known about the performance of these low temperature plastic materials in sCO₂, but experience in our autoclave system as well as discussions with others in industry has indicated a severe need in this area. We are completing a thorough review of literature on this topic, and developing a research plan for experimental activities that are needed to resolve this risk and better inform selection of these materials for low temperature system applications. Sandia's experience from Hydrogen Codes & Standards will be leveraged on sCO₂ systems (see examples below)

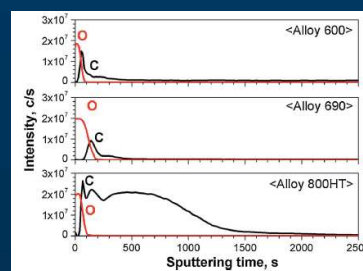


TENSILE STRENGTH FOR THERMOPLASTICS BEFORE AND AFTER HYDROGEN EXPOSURE



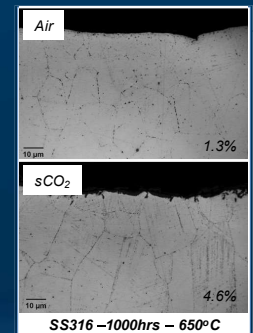
Structural Materials Consortium (Proposed)

Through extensive discussions with cross-cut collaborators (ORNL and UW-Madison), **alloy carburization has been identified as a critical materials risk for SFR EC systems.** Iron base alloys are more economical for SFR, but information is needed regarding C ingress at SFR temperatures. Mechanical properties are needed for both the base alloys and diffusion weld regions for the HX; it is critical to understand how these properties change when exposed to sCO₂ at temperature.



1000hrs - 600°C - 20 MPa sCO₂

Higher sub-surface carbon for Fe-base alloy versus for Ni-base alloys
Lee-KAIST 2015



Increased carbide precipitation in sCO₂
Olivares - CSIRO 2015



Task 1
Tensile performance of diffusion bonded Fe-base alloys

- (1) Perform baseline tensile testing on base metal and diffusion bonded alloys.
- (2) Repeat assessment of "aged" base metal and diffusion bonded samples that have been exposed to sCO₂ for a thousand hours.



Task 2
Cycle fatigue performance of diffusion bonded Fe-base alloys

- (1) Perform baseline fatigue assessment on base metal and diffusion bonded alloys.
- (2) Repeat assessment of "aged" base metal and diffusion bonded alloys that have been exposed to sCO₂ for a thousand hours.



Task 3
Effect of Cr and Ni contents on compatibility of Fe-base alloys in sCO₂ for SFR applications

- Quantify the oxide thickness and C ingress after 1,000 h of testing in 200 bar RG CO₂ as a function of alloy Cr and Ni contents to determine if composition affects compatibility in this temperature range