

A Markov Method for Simulating Non-Gaussian Wind Speed Time Series

Gerald M. McNerney, Paul S. Veers

Prepared by
Sandia National Laboratories
Albuquerque, New Mexico 87185 and Livermore, California 94550
for the United States Department of Energy
under Contract DE-AC04-76DP00789

Issued by Sandia National Laboratories, operated for the United States Department of Energy by Sandia Corporation.

NOTICE: This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government, any agency thereof or any of their contractors or subcontractors. The views and opinions expressed herein do not necessarily state or reflect those of the United States Government, any agency thereof or any of their contractors or subcontractors.

Printed in the United States of America
Available from
National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Road
Springfield, VA 22161

NTIS price codes
Printed copy: A02
Microfiche copy: A01

A MARKOV METHOD FOR SIMULATING NON-GAUSSIAN
WIND SPEED TIME SERIES*

Gerald M. McNerney
Wind America, Inc.

Paul S. Veers
Sandia National Laboratories
Albuquerque, NM 87185

ABSTRACT

This paper details a method which can be used to construct a wind simulator capable of generating wind time series with any distribution of hourly averages, exponentially decaying autocorrelation function, and a Gaussian realization of the turbulence. The method is based on a Markov random walk for hourly averages, and an inverse inverse hourly transform of the power spectrum to produce short-term turbulence. The Markov process is discussed in the first section and the turbulence generator is covered in the second section. A description of the applications for which the model was developed follows.

*This work supported by the US Department of Energy at Sandia National Laboratories under Contract No. DE-AC04-76DP00789.

INTRODUCTION

Wind speed time series may be periodic, random non-Gaussian or random Gaussian depending on the time scales involved. Monthly averages appear to have a strong periodic component over twelve months due to the seasonal changes in the global wind phenomenon. Hourly averages are a random process with a probability density which resembles a Weibull distribution. Instantaneous readings taken at one-second intervals strongly resemble a Gaussian random process. The purpose of this wind speed simulation is to provide input to a wind turbine generator control system simulation. The control system for a wind turbine has the task of deciding when to turn the turbine on or off to balance the energy capture with fatigue life consumption. This is currently accomplished by continually sampling the wind, usually at roughly one-second intervals, and using a predetermined algorithm to decide if the turbine should be on or off. The efficiency and protection from fatigue damage afforded by any particular algorithm is dependent on how it performs over a long period of time. Since high frequency wind speed data is not available for long times and a wide variety of wind sites, a wind speed simulation is necessary. The periodic nature of monthly averages is not modeled, but both the non-Gaussian hourly averages and the Gaussian high frequency wind speed variations are modeled.

The method of generating a sample of hourly averages is a Markov process random walk. A transition matrix relates each hourly average with the previous hourly average based upon 1) the desired probability density and 2) autocorrelation of the wind speed process. These two properties of the random process are uncoupled by defining the transition matrix as a normalized product of a diagonal probability matrix, to control the probability density, and a symmetric decay matrix, to control the autocorrelation. Thus, a series of hourly average wind speeds can be generated with any desired probability density function and an exponentially decaying autocorrelation with specified rate of exponential decay.

The high frequency wind speed time series, which represents the atmospheric turbulence, is superimposed on the hourly averages. The turbulence is represented as a Gaussian random process defined by its power spectral density (psd). This frequency domain representation of the turbulence is converted to the time domain using a fast Fourier transform which is computationally efficient. The functional form of the psd reflects changes in mean wind speed and permits adjustments to the turbulence intensity. A tapering scheme is employed to produce a smooth transition between adjacent hours.

GENERATING HOURLY AVERAGES

The basic method for generating a realization of hourly averages is a discrete time random walk over a finite state space of wind speeds. The process is Markovian in that the step to each succeeding state depends only on the preceding state and not on earlier states. Such a process may be represented by a matrix

$$[T] = \begin{bmatrix} t_{11} & t_{12} & \dots & t_{1m} \\ t_{21} & t_{22} & \dots & t_{2m} \\ \vdots & \vdots & \ddots & \vdots \\ t_{m1} & t_{m2} & \dots & t_{mm} \end{bmatrix} \quad (1)$$

called the transition matrix. In this representation, t_{ij} is the one-step probability of transition from state i to state j . The transition matrix must have the following two properties:

- i) all the entries are non-negative,
- ii) the sum of the entries in each row is one.

Any matrix with these properties is called a stochastic matrix. It is a useful fact that the product of any two stochastic matrices is a stochastic matrix.

The property of transition matrices that will be used is the so-called renewal theorem which implies that if $[T]$ is stationary, irreducible, and aperiodic, then $[T]$ has the ergodic property, which is

$$\lim_{M \rightarrow \infty} [T]^M = \begin{bmatrix} r_1 & r_2 & \dots & r_m \\ r_1 & r_2 & \dots & r_m \\ \vdots & \vdots & \ddots & \vdots \\ r_1 & r_2 & \dots & r_m \end{bmatrix} \quad (2)$$

where the limit is of the M th exponent of the transition matrix $[T]$, and the elements r_1, r_2, \dots, r_m constitute a probability vector $\{r\}$ called the limiting probability density function or limiting pdf (1). A transition matrix is stationary if it does not change in time, the irreducible property implies there are no closed or absorbing subsets of states, and a state is periodic if a random walk can return to that state only on integral multiples of the period.

The transition matrix can be used to represent a random walk since for a starting probability vector $\{v_0\}$, the n th step probabilities are given by the vector $\{v_n\} = \{v_0\} [T]^n$. To use $[T]$ in realizing a random walk, first form the cumulative distribution matrix $[C]$, where $c_{ij} = \sum_{k=1}^j t_{ik}$. Then when in the

state i , choose a random number R from a uniform distribution and the next state will be k , where

$$c_{ik-1} < R \leq c_{ik}$$

For our purposes, [T] needs to be ergodic with the limiting pdf equal to the pdf of hourly average wind speeds, and the resulting time series must have an exponentially decaying autocorrelation function with a specified rate of decay or, equivalently, a specified base.

To do this, define the transition matrix as the normalized product of two matrices, one to determine the probabilities of arriving in each state and the other to induce the desired autocorrelation property. A transition matrix can be found which will produce any combination of autocorrelation and pdf by varying these two matrices.

To begin the construction, the discrete weighting function $g_i = 2^{-|i|}$ is chosen and a decay matrix [G] is defined by

$$[G]_{ij} = g_{i-j} \quad (3)$$

The transition matrix is then defined as the matrix product

$$[T] = [N][G][P], \quad (4)$$

where [P] is the initial pdf matrix consisting only of diagonal entries p_1, p_2, \dots, p_m , and [N] is a diagonal normalization matrix with diagonals

$$1/n_i = 1/(\sum_k p_k g_{k-i}) \quad (5)$$

The elements of [T] are then

$$t_{ij} = g_{i-j} p_j / n_i \quad (6)$$

[T] has no zero entries so it is aperiodic and irreducible. Since [T] has no time dependence, it is also stationary and therefore ergodic and has a limiting pdf $\{r\} = (r_1, r_2, \dots, r_m)^T$. In practice, the initial pdf $\{p\}$ and the limiting pdf $\{r\}$ are different. In order that the limiting pdf be the desired result, the initial pdf must be compensated. This is done by first finding a functional form of the limiting pdf in terms of the initial pdf and then numerically inverting the relation.

To derive the relation between $\{r\}$ and $\{p\}$, an alternate form of $[T]^M$ will be given which is then compared with equation (2). First, observe that any power of [T] must have the form

$$T^M = [N][A]^{M-1}[P], \quad (7)$$

where $[A]^{M-1}$ is a symmetric matrix of the form

$$[A]^{M-1} = [G]([P][N][G])^{M-1} \\ = ([G][P][N])^{M-1}[G] \quad (8)$$

Since [T] is ergodic,

$$\lim_{M \rightarrow \infty} [T]^M = [N][A^\infty][P], \quad (9)$$

where the limit has the form of equation (2). Let the elements of

$$[A^\infty] \text{ be } A_{ij} = A_{ji}.$$

then

$$[N][A^\infty][P] = \begin{bmatrix} A_{11}p_1/n_1 & A_{12}p_2/n_1 & \dots & A_{1m}p_m/n_1 \\ A_{12}p_1/n_2 & A_{22}p_2/n_2 & \dots & A_{2m}p_m/n_2 \\ \vdots & \vdots & \ddots & \vdots \\ A_{1m}p_1/n_m & A_{2m}p_2/n_m & \dots & A_{mm}p_m/n_m \end{bmatrix} \quad (10)$$

Comparison with the limiting matrix in equation (2) reveals that

$$\begin{aligned} A_{11}/n_1 &= A_{12}/n_2 = \dots = A_{1m}/n_m = r_1/p_1 \\ A_{12}/n_1 &= A_{22}/n_2 = \dots = A_{2m}/n_m = r_2/p_2 \\ &\vdots \\ A_{1m}/n_1 &= A_{2m}/n_2 = \dots = A_{mm}/n_m = r_m/p_m \end{aligned} \quad (11)$$

Thus, all the A_{ij} 's can be solved in terms of one of them, say A_{11} , or

$$A_{ij} = n_i n_j A_{11} / n_1^2 \quad (12)$$

It follows that

$$r_j = A_{11} p_j n_j / n_1^2 \quad (13)$$

which has the proper form, i.e., no i dependence. Since the limiting matrix is stochastic and $\{r\}$ is a probability vector, it follows that

$$\sum_k r_k = (A_{11}/n_1^2) \sum_k p_k n_k = 1, \quad (14)$$

and thus

$$A_{11} = n_1^2 / \sum_k p_k n_k \quad (15)$$

With this form for A_{11} , the elements of $\{r\}$ can be solved for

$$r_j = p_j n_j / (\sum_k p_k n_k) \quad (16)$$

The product $p_j n_j$ can be expressed in vector form, which will be useful in inverting the equation for $\{r\}$, thus $\{r\}$ tentatively will be expressed as

$$\{r\} = [P][G]\{p\} \quad (17)$$

remembering that this product must be normalized to represent a probability.

Equation (17) may be used in an iterative process to find the initial pdf $\{p\}$ in terms of the limiting pdf $\{r\}$ which is known. First choose $\{p\}^0 = \{r\}$, then calculate

$$\{r\}^1 = [P]^0 [G] \{p\}^0 \quad (18)$$

Then normalize $\{r\}^1$ and calculate

$$\{p\}^1 = \{p\}^0 + F(\{r\} - \{r\}^1), \quad (19)$$

where $0 < F < 1$ is a relaxation factor which stabilizes the convergence. For successive steps use

$$\{r\}^n = \{p\}^{n-1} [G] \{p\}^{n-1} \quad (20)$$

$$\{p\}^n = \{p\}^{n-1} + F(\{r\} - \{p\}^n) \quad (21)$$

where $\{r\}^n$ must be normalized every step after equation (20). This process converges in 5 to 10 steps. The transition matrix can be calculated since the initial pdf is now known. However, the decay function has been arbitrarily chosen and the resulting autocorrelation may not have the desired rate of decay. To remedy this, a random walk must be conducted and the autocorrelation calculated. If the rate of decay is too fast, then change the decay function from $g_1 = 2^{-|i|}$ to $g_1 = B^{-|i|}$, where $B < 2$. If the decay is too slow, use $B > 2$, and repeat the process. All physically reasonable hourly autocorrelations can be reached by starting initially with $B = 2$ and $\Delta B = 0.4$, then bisecting in five steps. The autocorrelation of the random walk will never be an exact exponential but if the first two hours are matched to the exponential, the error on the 12th hour generally will be 10 to 20 percent with the simulated usually greater than exponential decay. This is beneficial in the sense that real wind autocorrelation deviates from the exponential in the same manner. The Markov process cannot be made to give a diurnal cycle. The procedure described above allows the operator to choose any combination of autocorrelation decay and limiting pdf.

As an example, a Markov process was constructed for a Rayleigh pdf with mean wind speed of 8 m/s and autocorrelation with exponential decay on a base of 0.87. The results of the walk are given in Table I. The first column is the wind speed in meters per second, the second column is the desired Rayleigh pdf, the third column is the pdf that was realized by the walk after 8760 steps, and the fourth column is the initial pdf that was calculated during the program. The first 20 rows and columns of the associated transition matrix with two significant figures for clarity of presentation are given in Table II. The χ^2 goodness-of-fit test was performed on the resulting distributions. It was found that the resulting pdf just passes at the 0.05 level of confidence, which is normally used with goodness-of-fit tests. Figure 1 is a plot of the first 1000 hours of the random walk on hourly averages.

TABLE 1. DESIRED AND REALIZED PDF'S

Wind Speed (m/s)	Rayleigh pdf	Realized pdf	Initial pdf
1	.0242	.0267	.0381
2	.0466	.0531	.0533
3	.0657	.0667	.0622
4	.0805	.0793	.0678
5	.0901	.0889	.0710
6	.0945	.0945	.0722
7	.0940	.0950	.0716
8	.0894	.0847	.0695
9	.0817	.0807	.0661
10	.0719	.0704	.0617
11	.0612	.0610	.0566
12	.0503	.0555	.0511
13	.0402	.0413	.0454
14	.0311	.0287	.0397
15	.0233	.0204	.0342
16	.0170	.0179	.0290
17	.0121	.0112	.0244
18	.0083	.0089	.0200
19	.0056	.0049	.0163
20	.0036	.0039	.0131
21	.0023	.0018	.0104
22	.0014	.0016	.0081
23	.0009	.0010	.0061
24	.0005	.0007	.0044
25	.0003	.0006	.0031
26	.0002	.0005	.0020
27	.0001	.0001	.0012

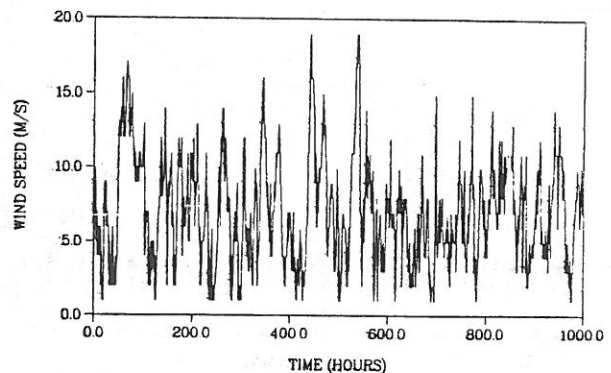


FIG. 1. 1000 HOURS OF A RANDOM WALK OF HOURLY AVERAGES

DISTRIBUTION:

Aerolite, Inc.
550 Russells Mills Road
South Dartmouth, MA 02748
Attn: R. K. St. Aubin

Alcoa Technical Center (4)
Aluminum Company of America
Alcoa Center, PA 15069
Attn: D. K. Ai

J. T. Huang
J. R. Jombock
Marshall Klingensmith
J. L. Prohaska

Alternative Sources of Energy
Milaca, MN 56353
Attn: Larry Stoiaken

Amarillo College
Amarillo, TX 79100
Attn: E. Gilmore

American Wind Energy Association
1516 King Street
Alexandria, VA 22314

Arizona State University
University Library
Tempe, AZ 85281
Attn: M. E. Beecher

R. G. Richards
Atlantic Wind Test Site
PO Box 189
Tignish P.E.I., COB 2B0
CANADA

Battelle-Pacific Northwest Laboratory
PO Box 999
Richland, WA 99352
Attn: Larry Wendell

Dr. George Bergeles
Dept. of Mechanical Engineering
National Technical University
42, Patission Street
Athens, GREECE

Bonneville Power Administration
PO Box 3621
Portland, OR 97225
Attn: N. Butler

Burns & Roe, Inc.
800 Kinderkamack Road
Oradell, NJ 07649
Attn: G. A. Fontana

Tom Watson
Canadian Standards Association
178 Rexdale Blvd.
Rexdale, Ontario, M9W 1R3
CANADA

Professor V. A. L. Chasteau
School of Engineering
University of Auckland
Private Bag
Auckland, NEW ZEALAND

Colorado State University
Dept. of Civil Engineering
Fort Collins, CO 80521
Attn: R. N. Meroney

Commonwealth Electric Co.
Box 368
Vineyard Haven, MA 02568
Attn: D. W. Dunham

Gale B. Curtis
Curtis Associates
3089 Oro Blanco Drive
Colorado Springs, CO 80917

M. M. Curvin
11169 Loop Road
Soddy Daisy, TN 37379

Department of Economic Planning
and Development
Barrett Building
Cheyenne, WY 82002
Attn: G. N. Monsson

Otto de Vries
National Aerospace Laboratory
Anthony Fokkerweg 2
Amsterdam 1017
THE NETHERLANDS

DOE/ALO
Albuquerque, NM 87115
Attn: G. P. Tennyson

DOE/ALO
Energy Technology Liaison Office
NGD
Albuquerque, NM 87115
Attn: Capt. J. L. Hanson, USAF

DOE Headquarters (20)
Wind Energy Technology Division
1000 Independence Avenue
Washington, DC 20585
Attn: L. V. Divone
P. Goldman

Dominion Aluminum Fabricating, Ltd. (2)
3570 Hawkestone Road
Mississauga, Ontario, L5C 2V8
CANADA
Attn: L. Schienbein
C. Wood

J. B. Dragt
Nederlands Energy Research Foundation
(E.C.N.)
Physics Department
Westerduinweg 3 Petten (nh)
THE NETHERLANDS

Dynergy Systems Corporation
821 West L Street
Los Banos, CA 93635
Attn: C. Fagundes

Dr. Norman E. Farb
10705 Providence Drive
Villa Park, CA 92667

Electric Power Research Institute
3412 Hillview Avenue
Palo Alto, CA 94304
Attn: E. Demeo
F. Goodman

Alcir de Faro Orlando
Pontificia Universidade Catolica-PUC/Rj
Mechanical Engineering Department
R. Marques de S. Vicente 225
Rio de Janeiro, BRAZIL

FloWind Corporation (4)
21414 68th Avenue South
Kent, WA 98031
Attn: Herman M. Drees
S. Tremoulet
I. E. Vas
R. Watson

Gates Learjet
Mid-Continent Airport
PO Box 7707
Wichita, KS 67277
Attn: G. D. Park

H. Gerardin
Mechanical Engineering Department
Faculty of Sciences and Engineering
Universite Laval-Quebec, G1K 7P4
CANADA

R. T. Griffiths
University College of Swansea
Dept. of Mechanical Engineering
Singleton Park
Swansea, SA2 8PP, UNITED KINGDOM

Helion, Inc.
Box 445
Brownsville, CA 95919
Attn: Jack Park, President

Institut de Recherche d'Hydro-Quebec
1800, Montee Ste-Julie
Varennnes, Quebec, JOL 2P0
CANADA
Attn: Gaston Beaulieu
Bernard Masse

Iowa State University
Agricultural Engineering, Room 213
Ames, IA 50010
Attn: L. H. Soderholm

Kaiser Aluminum and Chemical Sales, Inc.
14200 Cottage Grove Avenue
Dolton, IL 60419
Attn: A. A. Hagman

Kaiser Aluminum and Chemical Sales, Inc.
6177 Sunol Blvd.
PO Box 877
Pleasanton, CA 94566
Attn: D. D. Doerr

Kaman Aerospace Corporation
Old Windsor Road
Bloomfield, CT 06002
Attn: W. Batesol

Kansas State University
Electrical Engineering Department
Manhattan, KS 66506
Attn: Dr. G. L. Johnson

R. E. Kelland
The College of Trades and Technology
PO Box 1693
Prince Philip Drive
St. John's, Newfoundland, A1C 5P7
CANADA

KW Control Systems, Inc.
RD#4, Box 914C
South Plank Road
Middletown, NY 10940
Attn: R. H. Klein

Kalman Nagy Lehoczky
Cort Adellers GT. 30
Oslo 2, NORWAY

L. Liljidadhl
Building 005, Room 304
Barc-West
Beltsville, MD 20705

Olle Ljungstrom
FFA, The Aeronautical Research Institute
Box 11021
S-16111 Bromma, SWEDEN

Robert Lynette
R. Lynette & Assoc., Inc.
15921 SE 46th Way
Bellevue, WA 98006

Massachusetts Institute of Technology (2)
77 Massachusetts Avenue
Cambridge, MA 02139
Attn: Professor N. D. Ham
W. L. Harris, Aero/Astro Dept.

H. S. Matsuda
Composite Materials Laboratory
Pioneering R&D Laboratories
Toray Industries, Inc.
Sonoyama, Otsu, Shiga, JAPAN 520

Michigan State University
Division of Engineering Research
East Lansing, MI 48825
Attn: O. Krauss

Napier College of Commerce and Technology
Tutor Librarian, Technology Faculty
Colinton Road
Edinburgh, EH10 5DT, ENGLAND

NASA Lewis Research Center (2)
21000 Brookpark Road
Cleveland, OH 44135
Attn: D. Baldwin
J. Savino

National Rural Electric Cooperative Assn
1800 Massachusetts Avenue NW
Washington, DC 20036
Attn: Wilson Prichett III

Natural Power, Inc.
New Boston, NH 03070
Attn: Leander Nichols

Northwestern University
Dept. of Civil Engineering
Evanston, IL 60201
Attn: R. A. Parmalee

Ohio State University
Aeronautical and Astronautical Dept.
2070 Neil Avenue
Columbus, OH 43210
Attn: Professor G. Gregorek

Oklahoma State University
Mechanical Engineering Dept.
Stillwater, OK 76074
Attn: D. K. McLaughlin

Oregon State University (2)
Mechanical Engineering Dept.
Corvallis, OR 97331
Attn: R. W. Thresher
R. E. Wilson

Pacific Gas & Electric
3400 Crow Canyon Road
San Ramon, CA 94583
Attn: T. Hillesland

Ion Paraschivoiu
Department of Mechanical Engineering
Ecole Polytechnique
CP 6079
Succursale A
Montreal H3C 3A7 CANADA

Troels Friis Pedersen
Riso National Laboratory
Postbox 49
DK-4000 Roskilde, DENMARK

Helge Petersen
Riso National Laboratory
DK-4000 Roskilde, DENMARK

The Power Company, Inc.
PO Box 221
Genesee Depot, WI 53217
Attn: A. A. Nedd

Power Technologies Inc.
PO Box 1058
Schenectady, NY 12301-1058
Attn: Eric N. Hinrichsen

Public Service Co. of New Hampshire
1000 Elm Street
Manchester, NH 03105
Attn: D. L. C. Frederick

Public Service Company of New Mexico
PO Box 2267
Albuquerque, NM 87103
Attn: M. Lechner

RANN, Inc.
260 Sheridan Ave., Suite 414
Palo Alto, CA 94306
Attn: Alfred J. Eggers, Jr.
Chairman of the Board

Renewable Energy Ventures
190 South King Street, Suite 2460
Honolulu, HI 96813
Attn: G. W. Stricker

The Resources Agency
Department of Water Resources
Energy Division
PO Box 388
Sacramento, CA 95802
Attn: R. G. Ferreira

Reynolds Metals Company
Mill Products Division
6601 West Broad Street
Richmond, VA 23261
Attn: G. E. Lennox

A. Robb
Memorial University of Newfoundland
Faculty of Engineering and Applied Sciences
St. John's Newfoundland, A1C 5S7
CANADA

Rockwell International
Rocky Flats Plant
PO Box 464
Golden, CO 80401
Attn: Andrew Trenka (2)

Dr. Ing. Hans Ruscheweyh
Institut fur Leichbau
Technische Hochschule Aachen
Wullnerstrasse 7,
FEDERAL REPUBLIC OF GERMANY

Beatrice de Saint Louvent
Etablissement d'Etudes et de Recherches
Meteorologiques
77 Rue de Serves
92106 Boulogne-Billancourt Cedex,
FRANCE

Gwen Schreiner
Librarian
National Atomic Museum
Albuquerque, NM 87185

Arnan Seginer
Professor of Aerodynamics
Technion-Israel Institute of Technology
Department of Aeronautical Engineering
Haifa,
ISRAEL

David Sharpe
Dept. of Aeronautical Engineering
Queen Mary College
Mile End Road
London, E1 4NS UNITED KINGDOM

Kent Smith
Instituto Tecnológico Costa Rica
Apartado 159 Cartago,
COSTA RICA

Solar Initiative
Citicorp Plaza, Suite 900
180 Grand Avenue
Oakland, CA 94612
Attn: Jerry Yudelton

Bent Sorenson
Roskilde University Center
Energy Group, Bldg. 17.2
IMFUFA
PO Box 260
DK-400 Roskilde,

DENMARK

South Dakota School of Mines and Technology
Dept. of Mechanical Engineering
Rapid City, SD 57701
Attn: E. E. Anderson

Southern California Edison
Research & Development Dept., Room 497
PO Box 800
Rosemead, CA 91770
Attn: R. L. Scheffler

Southern Illinois University
School of Engineering
Carbondale, IL 62901
Attn: C. W. Dodd

G. Stacey
The University of Reading
Department of Engineering
Whiteknights, Reading, RG6 2AY,
ENGLAND

Stanford University
Dept. of Aeronautics and
Astronautics Mechanical Engineering
Stanford, CA 94305
Attn: Holt Ashley

R. J. Templin (3)
Low Speed Aerodynamics Laboratory
NRC-National Aeronautical Establishment
Montreal Road
Ottawa, Ontario, K1A 0R6, CANADA

Texas Tech University (2)
Mechanical Engineering Dept.
PO Box 4389
Lubbock, TX 79409
Attn: J. W. Oler
J. Strickland

Tulane University
Dept. of Mechanical Engineering
New Orleans, LA 70018
Attn: R. G. Watts

Tumac Industries, Inc.
650 Ford Street
Colorado Springs, CO 80915
Attn: J. R. McConnell

J. M. Turner
Terrestrial Energy Technology Program Office
Energy Conversion Branch
Aerospace Power Division/Aero Propulsion Lab
Air Force Systems Command (AFSC)
Wright-Patterson Air Force Base, OH 45433

United Engineers and Constructors, Inc.
PO Box 8223
Philadelphia, PA 19101
Attn: A. J. Karalis

University of Alaska
Geophysical Institute
Fairbanks, AK 99701
Attn: T. Wentink, Jr.

University of California
Institute of Geophysics
and Planetary Physics
Riverside, CA 92521
Attn: Dr. P. J. Baum

University of Colorado
Dept. of Aerospace Engineering Sciences
Boulder, CO 80309
Attn: J. D. Fock, Jr.

University of Massachusetts
Mechanical and Aerospace Engineering Dept.
Amherst, MA 01003
Attn: Dr. D. E. Cromack

University of New Mexico
New Mexico Engineering Research Institute
Campus PO Box 25
Albuquerque, NM 87131
Attn: G. G. Leigh

University of Oklahoma
Aero Engineering Department
Norman, OK 73069
Attn: K. Bergey

R. Camerero
University of Sherbrooke
Faculty of Applied Science
Sherbrooke, Quebec, J1K 2R1
CANADA

The University of Tennessee
Dept. of Electrical Engineering
Knoxville, TN 37916
Attn: T. W. Reddoch

USDA, Agricultural Research Service
Southwest Great Plains Research Center
Bushland, TX 79012
Attn: Dr. R. N. Clark

Utah Power and Light Co.
51 East Main Street
PO Box 277
American Fork, UT 84003
Attn: K. R. Rasmussen

W. A. Vachon
W. A. Vachon & Associates
PO Box 149
Manchester, MA 01944

VAWTPower, Inc.
134 Rio Rancho Drive
Rio Rancho, NM 87124
Attn: P. N. Vosburgh

Washington State University
Dept. of Electrical Engineering
Pullman, WA 99163
Attn: F. K. Bechtel

West Texas State University
Government Depository Library
Number 613
Canyon, TX 79015

West Texas State University
Department of Physics
PO Box 248
Canyon, TX 79016
Attn: V. Nelson

West Virginia University
Dept. of Aero Engineering
1062 Kountz Avenue
Morgantown, WV 26505
Attn: R. Walters

D. Westlind
Central Lincoln People's Utility District
2129 North Coast Highway
Newport, OR 97365-1795

Wichita State University
Aero Engineering Department (2)
Wichita, KS 67208
Attn: M. Snyder
W. Wentz

Wind Energy Report
Box 14
102 S. Village Avenue
Rockville Centre, NY 11571
Attn: Farrell Smith Seiler

Wind Power Digest
PO Box 700
Bascom, OH 44809
Attn: Michael Evans

Wisconsin Division of State Energy
8th Floor
101 South Webster Street
Madison, WI 53702
Attn: Wind Program Manager

1520	D. J. McCloskey
1522	R. C. Reuter, Jr.
1523	J. H. Biffle
1524	W. N. Sullivan
1524	P. S. Veers (10)
1524	D. W. Lobitz
1600	R. G. Clem
1630	R. C. Maydew
1636	J. K. Cole
2525	R. P. Clark
3141-1	C. M. Ostrander
3151	W. L. Garner (3)
3154-3	C. H. Dalin (28)
	For DOE/TIC (Unlimited Release)
3160	J. E. Mitchell (15)
3161	P. S. Wilson
6000	E. H. Beckner
6200	V. L. Dugan
6220	D. G. Schueler
6225	R. H. Braasch (50)
6225	T. D. Ashwill
6225	D. E. Berg
6225	R. D. Grover
6225	E. G. Kadlec
6225	P. C. Klimas
6225	M. T. Mattison
6225	R. O. Nellums
6225	D. S. Oscar
6225	M. E. Ralph
6225	M. H. Worstell
7111	J. W. Reed
7544	D. R. Schafer
7544	T. G. Carne
7544	J. Lauffer
8024	M. A. Pound

